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(54) **Resin composition and heat shrinkable film comprising the same composition layer.**

(57) A resin composition which comprises :
(i) 26 to 70 weight% of a thermoplastic polyester resin ;
(ii) 10 to 30 weight% of a polyester elastomer ;and
(iii) 20 to 44 weight% of a vinylidene chloride resin.

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This invention relates to a resin composition and to a biaxially stretched heat shrinkable film comprising at least one layer of the resin composition.

In general, shrink packaging is the most convenient form for uneven and irregularly shaped food products such as raw meat or processed meat. As the food packaging needs a long preservation period, it is not only
5 desired to have a superior oxygen gas barrier property [below 200 cc/m²·day·atm. at 30°C, under 100% RH], but also superior cold resistance.

Vinylidene chloride resin (PVDC) film is widely used with its superior oxygen gas barrier property, oil resistance, and clipping property besides its shrinkability. However, ordinary PVDC film sometimes has insufficient strength, especially under low temperatures (cold resistance) and under severe packaging conditions while
10 packaging heavy materials. It is desired to have a packaging material without these defects.

Resin compositions containing PVDC and a polyester copolymer resin derived from terephthalic acid and ethylene glycol and cyclohexane dimethanol are disclosed in US-A-4,725,651 and it is indicated that moldings thereof have a superior oxygen gas barrier property and mechanical strength.

However, the film made from the blended resin composition comprising PVDC and a polyester does not
15 have satisfactory cold resistance. Some attempts, therefore, have been carried out to obtain heat shrinkable films having a good oxygen gas barrier property and cold resistance by laminating a PVDC barrier layer with other resin layers. For example, three-layer films have been provided to improve the cold resistance. The film is co-extruded and has an intermediate PVDC layer containing an extremely small amount of or no additives such as plasticizers and stabilizers, and two outer layers, provided on both sides of the PVDC layer, of an ethylene-vinylacetate copolymer (EVA) having an adhesive property to PVDC and excellent cold resistance (CA-
20 A-982923).

On the other hand, a heat shrinkable laminated film which has one PVDC layer and has not only an oxygen gas barrier property and excellent cold resistance, but also high melt hole resistance, heat-resistant sealing property (the heat resistance of a seal portion), and transparency after shrinking, is also required, especially
25 for packaging of fatty foods such as processed meat and cheese. The packaging and sterilization of fatty foods often involves problems in that a film softened by oil and heat may be stretched so that it becomes thin and breaks (a melt hole) and in that a sealed part or parts in the vicinity thereof may break due to heat shrinkage stress during sterilization. It is therefore desired to have a heat shrinkable film which has not only an oxygen gas barrier property, but also melt hole resistance, good heat resistance sealing property, sufficient cold resistance without pinholes occurring during low temperature distribution, and superior transparency after shrink-
30 ing.

As these heat shrinkable laminated films, laminates crosslinked by electron beams are used. For example a flexible laminate suitable for heat shrinkable packaging contains (1) a first layer containing an organic polymer, (2) an oxygen gas barrier layer based upon PVDC, having an oxygen gas transmission rate of lower
35 than 70 cc/m²·day·atm., in oxygen gas transmission rate of the laminated film (following ASTM Standard D1434, at 22.8°C and 0% RH), and (3) a layer containing an organic polymer having abuse endurance. This three layer laminated film is described in US-A-3,741,253 with the following embodiment. A laminate has a first layer (1) containing an oriented copolymer, crosslinked by irradiation, of ethylene and vinylacetate having 5 to 20 weight% units derived from the vinylacetate; an oxygen gas barrier layer (2) containing 70 to 85 weight% units
40 derived from vinylidene chloride and 30 to 15 weight% units derived from vinyl chloride; and a layer (3) consisting of (i) a copolymer of ethylene and vinylacetate having 5 to 20 weight% units derived from vinylacetate; and (ii) a polymer blend of isotactic polypropylene, atactic polypropylene, and polybut-1-ene.

US-A-4,699,846 discloses an improvement of the peeling off resistance among layers of a laminated film having (1) base film layer containing an α -mono olefin polymer which has been irradiated and crosslinked; and
45 (2) a film layer containing a polymer which has been crosslinked by the irradiation, the whole film comprising layers (1) and (2) being then irradiated to produce further crosslinking and stretched to attain the object described above.

JP-A-3948/1987 discloses heat shrinkable biaxially stretched multilayer film suitable for packaging slices of primal and subprimal meat and processed meat, comprising a vinylidene chloride-methylmethacrylate
50 copolymer as an oxygen gas barrier layer and irradiated with a 1 to 5 Mega rad dose. JP-A-23752/1987 discloses a molecular oriented multilayer polymer film having a first layer and a second layer consisting mainly of an ethylene vinylacetate copolymer and a layer of PVDC disposed therebetween, each composition being irradiated by an electron beam of over 1.5 Mega rad to attain crosslinking. However, when the resin composition in US-A-4,725,651 is used as a single layer of a heat shrinkable film having an oxygen gas barrier property
55 and cold resistance, it has inferior pin-hole resistance at the low temperature adopted in food distribution because of the high glass transition temperature of the polyester copolymer and also has low productivity due to violent degradation of the resin during extrusion molding.

A EVA/PVDC/EVA composition provides a superior laminated heat sealable film having cold resistance

and a good oxygen gas barrier property and compensates for the defects of a PVDC single layer product, but it has poor melt hole resistance and heat sealing resistance. Furthermore, the stretching is done at a temperature of not over 40° less than the crystal melting point of the polyolefin, to give shrinkability to a pair of polyolefin layers on both side of the PVDC layer, so the PVDC layer is not given enough stretching and orienting. Therefore, the heat shrinkability of the PVDC layer is deficient, and when the laminate is heat shrunk the PVDC layer is left behind and contains fine wrinkles. As a result, the laminate film has extremely poor transparency after shrinking.

It is strongly desired, therefore, in the food packaging field, to provide a heat shrinkable laminated film with excellent transparency after shrinking, having not only an oxygen gas barrier property and excellent cold resistance, but also excellent melt hole resistance and heat resistance sealing property. We have found a heat-shrinkable film which satisfies all the above demands.

The present invention provides a resin composition which comprises:

- (i) 26 to 70 weight% of a thermoplastic polyester resin;
- (ii) 10 to 30 weight% of a polyester elastomer; and
- (iii) 20 to 44 weight% of a vinylidene chloride resin.

The present invention also provides a biaxially stretched heat-shrinkable film having an oxygen gas barrier property which comprises a composition as defined above.

The present invention additionally provides a biaxially stretched heat shrinkable laminated film having a heat shrinkage percentage of over 15% at 90°C and an oxygen gas barrier property, which comprises an intermediate oxygen gas barrier layer comprising a composition as defined above, an outer layer of a polyamide or crosslinkable polyolefin, an inner layer of the same crosslinkable polyolefin used in the outer layer or a different polyolefin, and a heat sealing layer of a low crosslinkable polyolefin, at least the outer layer, the inner layer and the heat sealing layer being crosslinked by electron beam irradiation.

The laminated film has not only an oxygen gas barrier property and excellent cold resistance, but also excellent melt hole resistance, heat sealing resistance and superior transparency after shrinking.

The present invention further provides a process for producing a film as defined above, which comprises either extruding the composition defined above to form a film and biaxially stretching the film or coextruding the compositions forming the respective layers to form a film, crosslinking the layers by means of electron beam irradiation, preferably at 1 to 12 Mega rad, and biaxially stretching the film.

The present invention also provides the use of a film as defined above in packaging an article.

The present invention additionally provides a process for preparing a composition as defined above which comprises mixing together the thermoplastic polyester resin, the polyester elastomer and the vinylidene chloride resin.

The resin composition in this invention comprises 26 to 70 weight%, preferably 36 to 65 weight% of a thermoplastic polyester resin, 10~30 weight%, preferably 10~20 weight% of polyester elastomer, and 20~44 weight%, preferably 25~44 weight%, of PVDC.

Relating to the thermoplastic polyester resin, terephthalic acid, isophthalic acid, orthophthalic acid, adipic acid, sebacic acid, fumaric acid, maleic acid, trimeritic acid, succinic acid, benzene dicarboxylic acid, dodecan dicarboxylic acid, naphthalene dicarboxylic acid, diphenyl dicarboxylic acid, 2,2-bis(4-carboxyphenyl)propane, bis(4-carboxyphenyl)methane, and cyclohexane dicarboxylic acid are used as dibasic acid components and dialkyl esters derived from these acids (with alkyl group having 1 to 4 carbon atoms) are also used for this purpose.

And straight chain dialcohol compounds are favorable as dialcohol components, for example, ethylene glycol, propylene glycol, butylene glycol, neopentyl glycol, hexane diol, cyclohexane diol, diethylene glycol, triethylene glycol, tetraethylene glycol, and polyethylene glycol can be used for this purpose. The polyester resin derived from a mixture of terephthalic acid and isophthalic acid as dibasic acid and alcohols described above as alcohol component, and having 0.5~0.7 dl/gr in its intrinsic viscosity (lv value), with 0.5 gr/100 ml trifluoroacetic acid solution at 30°C, is used favorably among these polyester resins. And favorable ratio on the mixture of terephthalic acid and isophthalic acid is 55~90 mol% of terephthalic acid and 45~10 mol% of isophthalic acid.

Further, favorable polyester resin is derived from terephthalic acid and isophthalic acid as mixed dibasic acid and ethylene glycol and diethylene glycol as mixed dialcohol component with the ratio of 60~98 mol% of ethylene glycol and 2~40 mol% of diethylene glycol. Favorable polyester resin used in this invention should not be compatible with PVDC each other and preferable example is Kanebo Corporation's product, "PIFG-40" which is a copolymer resin of terephthalic acid-isophthalic acid-ethylene glycol-diethylene glycol, having 68°C of its glass transition temperature. If the content of polyester resin exceeds 70 weight%, the ratio of polyester elastomer becomes small value which makes insufficient cold resistance and if the content of polyester resin is below 21 weight%, polyester resin component can not be matrix. As polyester elastomer, polyester-polyether

copolymer which is derived from followings as main component, is preferably used:

- (i) dicarboxylic acid,
- (ii) lower glycol,
- (iii) higher glycol.

The component, (i) is selected from the aromatic dicarboxylic acids including terephthalic acid, isophthalic acid, phthalic acid, p-oxybenzoic acid, m-oxybenzoic acid, naphthalene dicarboxylic acid etc. and among the aliphatic dicarboxylic acids and alicyclic dicarboxylic acids including oxalic acid, adipic acid, succinic acid, sebacic acid, 1,4-cyclohexane dicarboxylic acid, 1,3-cyclohexane dicarboxylic acid etc. The component, (ii) is selected from such aromatic, aliphatic and alicyclic glycols as 1,4-butanediol, ethylene glycol, propylene glycol, hexamethylene glycol, neopentyl glycol, p-xylene glycol, cyclohexane glycol, alicyclic glycol etc. The component, (iii) is selected from polyethylene glycol, polypropylene glycol, polytetramethylene glycol, copolymer of these glycol etc., preferably the compounds having 8~20 carbon atoms as the ethylene segments.

Favorable example of polyester elastomer used in this invention is a copolymer resin derived from terephthalic acid-isophthalic acid-1,4-butanediol-polytetramethylene glycol [for example, Toray-Dupont's product, "HYTREL" #2501].

Though polyester elastomer has a role to add flexibility to the 3 component mixed resin, it can not give desirable cold resistance below 10 weight% content and is unfavorable to arise poor optical transparency and poor oxygen gas barrier property over 30 weight% content. A weight-average molecular weight of the polyester elastomer used in this invention is preferably about $0.5 \times 10^4 \sim 3 \times 10^4$, more preferably $0.8 \times 10^4 \sim 2.5 \times 10^4$.

As these polyester elastomers are added with their suitable amounts, the mixture of PVDC, polyester resin, and polyester elastomer can improve surprisingly the cold resistance without injuring the transparency.

The PVDC is preferably a copolymer composed of vinylidene chloride as a main component and a monomer which is copolymerizable with vinylidene chloride and especially, it is favorable to be 65~95 weight% in vinylidene chloride content. If the content of vinylidene chloride is below 65 weight%, it is not suitable for practical use, because of extreme deterioration on oxygen gas barrier property with becoming rubber like material at ordinary temperature and losing its crystal structure. And over 95 weight% in vinylidene chloride content, stable melt extrusion processing becomes difficult, because raising the melting point lead easily to its decomposition.

Concerning the monomer being copolymerizable with vinylidene chloride monomer, one or more than 2 kind unsaturated monomers are selected from following monomers: vinyl chloride, acrylonitrile, acrylic acid, methacrylic acid, alkylacrylate having 1~18 carbon atoms in alkyl group, alkylmethacrylate having 1~18 carbon atoms in alkyl group, maleic anhydride, maleic acid, alkylmaleate, itaconic acid, alkylitaconate, vinyl acetate, ethylene, propylene, isobutylene, butadiene, etc.

It is possible to add plasticizer and stabilizer into PVDC, if they are necessary. Each 0.1~3 weight% of plasticizer and stabilizer respectively, are favorable to add into PVDC and the amount below 0.1 weight% does not show their effects. Also, the amount over 3 weight%, injure the oxygen gas barrier property and can not attain the purpose of present invention.

Concerning stabilizer, specifically, epoxy type stabilizer is favorable, though heat stabilizer in the market can be used.

Following epoxy type stabilizers are illustrated for this purpose: epoxidized vegetable oil derived from soybean oil, safflower oil, sunflower oil, linseed oil, cotton seed oil etc. and epoxidized fatty oil monoester represented by epoxidized octyl stearate, epoxidized fatty acid diester obtained by epoxidation to glycolester of unsaturated fatty acid, alicyclic epoxide represented by epoxy hexahydro phthalic acid diester etc.

The resin composition comprising polyester, polyester elastomer, and PVDC which is described above, are processed with melt extrusion using extruder under ordinary method, and biaxially stretched with inflation, or biaxially stretched after press molding, T-die oxygen gas barrier property and cold resistance is formed. It is desirable that the product has heat shrinking percentage of over 20% at 90°C. Also, it is desirable that when the resin composition is used as the single layer film its thickness is preferably 8~100µm, more preferably 10~60µm.

In this invention, the film is stretched in the stretching ratio of over 2 times in the direction of length and breadth respectively by the ordinary biaxial stretching method, and so PVDC particles are stretched and dispersed in the matrix of polyester resin and polyester elastomer to long and slender particles and form a lot of flat layer in parallel with stretching direction (microlayer state). Accordingly, its oxygen gas barrier property is superior to non-stretching film.

If the content of PVDC is below 20 weight%, the film shows poor oxygen gas barrier property, and over 44 weight%, the film shows unfavorable colouring caused by degradation followed electron beam irradiation.

Also, in the blending of PVDC and only polyester elastomer which has compatibility with PVDC, as micro-layer condition is not attained, improvement on oxygen gas barrier property is not attained during biaxial stretching process.

The resin composition in this invention can be used as oxygen gas barrier layer in biaxially stretched heat

The resin composition in this invention can be used as oxygen gas barrier layer in biaxially stretched heat shrinkable laminated film. Related to the heat shrinkable laminated film, the favorable product is that the product comprises intermediate barrier layer prepared by the resin composition in this invention, outer layer from polyamide or polyolefin with crosslinking property, inner layer from polyolefin with crosslinking property made by the same or different material from the said outer layer, and heat sealing layer made by polyolefin with low crosslinking property. And moreover, the favorable product should be the one which at least the outer layer, inner layer, and heat sealing layer are crosslinked by the electron beam irradiation and has over 15% of its heat shrinkage percentage at 90°C.

Concerning polyamide resin used as the outer layer, the product having its melting point below 210°C, preferably below 180°C, is used for this purpose. The crystalline melting point of this polyamide is determined based upon the method of ASTM-D648. At least, one polyamide selected from aliphatic polyamides (4~12 in carbon atoms), alicyclic polyamides, and aromatic polyamides is preferably used. Followings are favorable monomers to constitute the polyamides, so the polymers and copolymers formed from these monomers are used for this purpose, for example, straight chain ω -amino carboxylic acid having 6~12 in its carbon atoms and its lactum, adipic acid, sebacic acid, dodecan dicarboxylic acid, heptadecan dicarboxylic acid, hexamethylene diamine, isophthalic acid, bis-(4-aminocyclohexyl)-methane, 2,2-bis-(4'-aminocyclohexyl)-propane, terephthalic acid and its dimethyl ester, 1,6-diamino-2,2,4-trimethylhexane, 1-amino-3-aminomethyl-3,5,5-trimethyl-cyclohexane etc. The most suitable materials among these polyamide or copolyamide are nylon 6-66, nylon 6-69, nylon 6-11, nylon 12, nylon 6-12, nylon 6-66-610, nylon 6-66-610-612 etc.

The polyamide resin having over 210°C in its crystalline melting point, requires higher processing temperature during melting extrusion of the laminate, so it brings difficulty about processing because PVDC is apt to decompose in processing temperature.

Relating to polyolefin having crosslinking property and used for outer or inner layer, one material used for this purpose is at least one polyolefin selected from following components: ethylene-vinylacetate copolymer (EVA, preferably, 5~20 weight% in vinylacetate content), ethylene-(meth)acrylic acid copolymer [Preferably, 5~20 weight% in (meth)acrylic acid content], ethylene-(meth)acrylate copolymer [preferably, 5~20 weight% in (meth)acrylate content], ethylene-(meth)acrylic acid allyl copolymer [0.005~2 mol%, preferably 0.01~1.0 mol% in (meth)acrylic acid allyl content], ethylene-vinylacetate-(meth)acrylic acid allyl copolymer resin [5~20 weight% in vinylacetate content and 0.005~2 mol%, preferably 0.01~1.0 mol% in (meth)acrylic allyl acid content], ethylene- α -olefin-(meth)acrylic allyl acid copolymer resin (propylene, butene-1, pentene-1, hexene-1, 4-methylpentene-1, octene-1, decene-1 etc. and the mixture of these are used as α -olefin), ethylene-1,4-diene copolymer resin, ethylene-propylene-1,4-diene copolymer resin, linear low density polyethylene by gas phase polymerization, ionomer resin etc. In these descriptions, (meth)acrylic acid designates acrylic acid or methacrylic acid.

As polyolefin with low crosslinking property for heat sealing layer in the most inner layer (the side contacting to the content packed), the suitable material, one or some mixtures, are selected from the followings: linear low density polyethylene (LLDPE) by solution polymerization method, ethylene-propylene copolymer resin, propylene-butene copolymer resin, low density polyethylene etc. Polyolefin having low crosslinking property means that the polyolefin shows comparatively difficulty to be crosslinked under the same level of electron beam irradiation, compared with said crosslinkable polyolefin. By the use of these polyolefins, application range on heat sealability is widened by this irradiation and the seal strength is improved greatly compared with non-irradiated one, and on the other hand, heat sealability is not decreased by the excess crosslinking.

As adhesives used in adhesive layer, followings are illustrated: α -olefin polymer derivatives, for example, graft polymer and its salt produced by graft polymerizing polyethylene or polypropylene with unsaturated carboxylic acid or its anhydride, α -olefin-vinylacetate copolymer or its derivatives and α -olefin-unsaturated carboxylic acid copolymer or its derivatives, for example, ethylene-(meth)acrylic acid copolymer, ethylene-(meth)acrylic acid alkyl ester copolymer and graft polymer and its salt produced by graft polymerizing any of these polymer with unsaturated carboxylic acid or its anhydride. As unsaturated carboxylic acid or its anhydride used for graft polymerization, acrylic acid, methacrylic acid, maleic acid, maleic anhydride etc. are used and favorable amount is 0.01~5 weight% to original polymers to be grafted. As especially favorable adhesive polymer, followings are illustrated: the graft polymers produced by graft polymerizing ethylene ethylacrylate copolymer (EEA) having 5~25 weight% in its ethylacrylate content or ethylene-vinylacetate copolymer having 5~25 weight% in its vinylacetate content with 0.05~0.5 weight% maleic anhydride.

These adhesive layer can be crosslinked by electron beam irradiation to make strong adhesion onto adjacent layer.

The expression "being crosslinked" made in this invention, means that the gel% value, an indication as the degree of crosslinking and being explained in later, is over 5%. The range of favorable gel% is 20~80%.

preferably 30~80%, in both outer and inner layers. The value below 20% has poor improvement result on melt hole resistance. Also, the favorable value is 10~40%, more preferably in the range 10~30% in heat sealing layer. The desirable value of heat sealing layer is below 40%, because too higher crosslinking degree produce poor sealing strength.

The dose level of electron beam irradiation is 1~12 Mega rad, preferably in the range of 1~10 Mega rad. Irradiation dose level below 1 Mega rad shows too small crosslinking, so it can not obtain the effect of crosslinking. And the irradiation dose level over 12 Mega rad is unfavorable because it arises coloring of laminated film and lowering of sealing strength caused by excess crosslinking in heat sealing layer.

Referring to laminated film in this invention, favorable thickness is 5~30 μm in outer and inner layer. Outer layer over 30 μm is unfavorable to cause unstable film production derived from too large stress during stretching.

Favorable thickness is 5~20 μm for oxygen gas barrier layer and the value below 5 μm is not desirable because of insufficient oxygen gas barrier effect.

Favorable thickness is 5~30 μm for the most inner layer, that is, heat sealing layer. Desirable thickness is 1~5 μm for adhesive layer.

Favorable thickness is 25~125 μm on total laminated film. The layer construction in the laminated film in this invention, can be shown outer layer/intermediate layer/inner layer/heat sealing layer or outer layer/inner layer/intermediate layer/heat sealing layer and, if it is necessary, adhesive layer can be placed between each layers or on both sides of intermediate layer.

The content packed contacts to the heat sealing layer which is the most inner layer, the outer layer corresponds to another most outer layer, and both intermediate and inner layers are existed between outer layer and heat sealing layer.

These laminated films become heat shrinkable film having over 15% in their heat shrinkage percentage at 90°C, by biaxial stretching process. The field of said laminated film being effectively used, is to package uneven and irregular fatty foods like raw red meat, processed meat, and cheese, and the heat shrinkage percent below 15% at 90°C, of used film is unfavorable to lower extremely commodity value because of the lack of tight contact to the content packed and the occurrence of separation of meat juice. Concerning oxygen barrier property on this packaging, necessary oxygen gas transmission rate is below 200 $\text{cc}/\text{m}^2\text{-day-atm}$, preferably below 100 $\text{cc}/\text{m}^2\text{-day-atm}$. The oxygen gas transmission rate over 200 $\text{cc}/\text{m}^2\text{-day-atm}$ is unfavorable to shorten the preservation period on the content and lose good commodity appearance.

Following is one of examples to manufacture biaxially stretched heat shrinkable laminated film in this invention. The mixture blended PVDC powder, polyester elastomer, and polyester resin pellet with prescribed ratio as oxygen gas barrier layer (intermediate layer), crosslinkable polyolefin resin used as outer and inner layer, and low crosslinkable polyolefin resin as heat sealing layer, are melted with adhesive resin, if necessary, respectively using plurality of extruders under ordinary process, then introduced into circular die to form laminate and laminated in the order of outer layer/adhesive layer/oxygen gas barrier layer/adhesive layer/inner layer/heat sealing layer by coextrusion. After the melt tubular film obtained is then quenched by a cooling water shower at 10~20°C, a flat tubular film is formed. The thus obtained tubular film is introduced into electron beam irradiation equipment, irradiated whole laminate layers with 1~12 Mega rad in its dose level, and then the over 2.5 times stretching was done in both direction of length and breadth respectively with inflation method at 50~120°C under simultaneous biaxial stretching. In this case, it is desirable to equally irradiate from the both surface of the flat tubular film so as to get homogeneous irradiation dose on the whole flat film thickness of flat tubular film.

The electron beam used in this invention, is a beam having 150~1000 KeV energy emitted from various electron accelerators including Cockroft-Walton's type, Van de Graaf type, Resonance transformer type, Insulation core transformer type, Linear accelerator type, Dynamitron type, High frequency cyclotron type etc.

Resin composition in this invention are mixture of PVDC, thermoplastic polyester resin, and polyester elastomer with specified ratio and show excellent oxygen gas barrier property, cold resistance and transparency, when these resin compositions are used for heat shrinkable film. Namely, as the suitable amount of polyester elastomer is added, it does not harm the transparency and can improve the cold resistance. And PVDC in blend resin into oxygen gas barrier layer, is lowered below 44 weight% in its weight ratio, and said oxygen gas barrier layer is stretched, so PVDC particle is dispersed to microlayer state of long and slender shape and can improve the oxygen gas barrier property, moreover it has an advantage of no-colouring without decomposition even under the irradiation of electron beam.

Biaxially stretched heat shrinkable laminated film which contains the layer comprising this resin compositions as oxygen gas barrier layer, is irradiated by electron beam, and at least outer layer, inner layer, and heat sealing layer were crosslinked, so further following effects are added to the effects described above.

(1) Oxygen gas barrier layer can be protected from abuse.

(2) Heat resistance of said laminated film can be improved surprisingly for improvement on heat resistance

of polyolefin layer affected by electron beam irradiation.

(3) As low crosslinkable polyolefin resin is used in heat sealing layer, the range of suitable heat sealing temperature is wide and sealing strength is greatly improved compared with non-irradiation film by electron beam.

5 (4) When adhesive layers are provided, the adhesive layers are also crosslinked, so turbidity which is caused by sliding among each layers even if the film is boiled at the temperature near boiling water can be prevented and film transparency is kept after boiling.

As these results, we have obtained heat shrinkable laminated film which keeps favorable oxygen gas transmission rate below 200 cc/m²·day·atm, melt hole property [damaged number 0 among 5 samples], haze below 10 8%, and seal strength over 1.8 kg/15 mm.

This invention is explained concretely using examples in following description but not restricted by these examples.

Example 1

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As resin composition the following resin composition A is used. The blended resin, A consists of 30 weight% of polyester resin having 68°C in its glass transition temperature and identified terephthalic acid-isophthalic acid-ethylene glycol-diethylene glycol copolymer resin (lv=0.52, PIFG-40 manufactured by Kanebo, Ltd.), 30 weight% of polyester elastomer identified terephthalic acid-isophthalic acid-1,4-butandiol-polytetramethyleneglycol copolymer resin (HYTREL #2501 manufactured by Toray-Dupont), 40 weight% of vinylidene chloride-methylacrylate copolymer resin (94% vinylidene chloride content), and 2 weight% of epoxidized soybean oil to said copolymer resin.

The resin composition A was mixed and melted using monoaxial extruder (cylinder diameter 40 mm, L/D=24) and prepared into pellet at 180°C resin temperature. The pellet was pressed to make test pieces, 500 25 µm in its thickness, with desk press (AYSR 5, Shinto Metal Works) at 180°C (50 kg/cm², 2 min.), then the test pieces were stretched 3.5 times in the direction of both length and breadth at 90°C into 40 µm film with biaxial stretching.

Example 2

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A biaxially stretched film was produced in the same way as that employed in Example 1, except that resin composition was adopted for following resin composition K. The resin composition K was a blended resin consisting of 45 weight% of PIFG-40 as polyester resin, 15 weight% of HYTREL #2501 as polyester elastomer, 40 weight% of vinylidene chloride-methylacrylate copolymer resin (94 weight%, vinylidene chloride content), 35 and 2 weight% of epoxidized soybean oil to said copolymer resin.

Example 3

A biaxially stretched film was produced in the same way as that employed in Example 1, except that resin 40 composition was adopted for following resin composition T. The resin composition T was a blended resin consisting of 50 weight% of PIFG-40 as polyester resin, 10 weight% of HYTREL #2501 as polyester elastomer, 40 weight% of vinylidene chloride-methylacrylate copolymer resin (94 weight%, vinylidene chloride content), and 2 weight% of epoxidized soybean oil to said copolymer resin.

Example 4

A biaxially stretched film was produced in the same way as that employed in Example 1, except that resin composition was adopted for following resin composition. The resin composition was a blended resin consisting of 65 weight% of PIFG-40 as polyester resin, 13 weight% of HYTREL #2501 as polyester elastomer, 22 weight% 50 of vinylidene chloride-methylacrylate copolymer resin (94 weight%, vinylidene chloride content), and 2 weight% of epoxidized soybean oil to said copolymer resin.

Comparative Example 1

55 A biaxially stretched film was produced in the same way as that employed in Example 1, except that resin composition was adopted for following resin composition S. The resin composition S was a blended resin consisting of 60 weight% of PIFG-40 as polyester resin, 40 weight% of vinylidene chloride-methylacrylate copolymer resin (94 weight%, vinylidene chloride content), and 2 weight% of epoxidized soybean oil to said

copolymer resin.

Comparative Example 2

A biaxially stretched film was produced in the same way as that employed in Example 1, except that resin composition was adopted for following resin composition. The resin composition was a blended resin consisting of 20 weight% of PIFG-40 as polyester resin, 40 weight% of HYTREL #2501 as polyester elastomer, 40 weight% of vinylidene chloride-methylacrylate copolymer resin (94 weight%, vinylidene chloride content), and 2 weight% of epoxidized soybean oil to said copolymer resin.

Comparative Example 3

A non-stretched press sheet having 500 μm thickness was produced in the same way that employed in Example 3, except that the sheet was not biaxially stretched. Impact thrusting energy and oxygen gas transmission rate were measured in sheet of 500 μm thickness and converted to the value of thickness of 40 μm (impact thrusting energy) and 8 μm (oxygen gas transmission rate).

Comparative Example 4

A biaxially stretched film was produced in the same way as that employed in obtained following the same Example 1, except that only polyester, PIFG-40 was used instead of resin composition.

Comparative Example 5

A biaxially stretched film was produced in the same way as that employed in Example 1, except that vinylidene chloride-methylacrylate copolymer resin (94 weight%, vinylidene chloride content) and 2 weight% of epoxidized soybean oil to said copolymer resin were used instead of resin composition.

Table 1 shows the data of heat shrinkage percentage, oxygen gas transmission rate (converted to 8 μm film thickness), and impact thrust energy of the film gained in Example 1~4 and Comparative Example 1~5. Table 4 shows the methods on measurement of the physical properties.

By this invention, excellent heat shrinkable film having good oxygen gas barrier property and cold resistance was obtained as clarified by Example 1~4. In general, heat shrinkable film with single layer being applicable for practical use requires heat shrinkage percent of over 20% in the direction of both length and breadth, oxygen gas transmission rate of below 100 $\text{cc/m}^2\text{-day-atm}$ (converted to 8 μm , 30°C, 100%RH), and impact thrusting energy of over 80 $\text{mJ/40 } \mu\text{m}$. While, Comparative Example 1 shows inferior impact strength (expressed by impact thrust energy) because of no content on polyester elastomer, Comparative Example 2 shows inferior oxygen gas barrier property because of beyond the limits on the content of polyester and polyester elastomer, Comparative Example 3 shows poor oxygen gas barrier property because of non-stretched film, and each Comparative Example 4, 5 show poor oxygen gas barrier property and cold resistance because of sole polyester and PVDC film respectively.

Table 1

	Resin Composition			Heat shrinkage Percentage L/T %	Oxygen gas transmission rate (cc/m ² ·day·atm)	Impact thrusting energy 5°C mJ/40 μm
	Polyester (%)	Polyester elastomer (%)	PVDC (%)			
Example 1	30	30	40	42/45	70	170
Example 2	45	15	40	45/45	65	150
Example 3	50	10	40	45/45	60	130
Example 4	65	13	22	43/43	80	140
Comparative Example 1	60	0	40	44/45	55	22
Comparative Example 2	20	40	40	45/45	120	260
Comparative Example 3	50	10	40	0/0	230	130
Comparative Example 4	100	0	0	30/25	410	30
Comparative Example 5	0	0	100	46/45	8	10

Example 5

① Resin composition A in Example 1 was used for the intermediate layer (oxygen gas barrier layer).

② Following resin composition B was used for outermost layer. The resin composition B was a blended resin consisting of each linear low density polyethylene (DFDA1137, manufactured by Nippon Unicar Co., Ltd. melt index = 1.0, density = 0.906 g/cm³) and EVA including 7.5 weight of vinylacetate content (NUC #8425 manufactured by Nippon Unicar Co., Ltd., melt index = 2.3, density = 0.93 g/cm³) with blending ratio 70:30 respectively.

③ Resin composition B was used as inner layer.

④ Resin C, low density polyethylene resin (F277-1 manufactured by Sumitomo Chemical Co., Ltd., melt index = 2.0, density = 0.924 g/cm³) was used as sealing layer.

⑤ Resin D, ethylene-ethylacrylate copolymer resin containing 15 weight% of ethylacrylate (DPDJ#6182, manufactured by Japan Unicar Company, melt index = 1.5, density = 0.93 g/cm³) was used as adhesive layer.

These resins A, B, C, D, were extruded separately with each 5 extruders, introduced with melted condition into circular die of coextruder, and coextruded to 7 layers construction shown in Table 2. The resin temperature of melted tubular film was 190°C at die outlet portion. Said melted tubular film was quenched by showering with water at 10~30°C and changed into flat tubular film having 150 mm in flat width and 510 μm in its thickness.

The thus obtained flat tubular film was irradiated with 10 Mega rad in electron irradiation equipment having 400 KeV of accelerating voltage. Next, the film was passed through hot water bath at 80~95°C and hot wind cylinder at 110°C and stretched each 3 times in the direction of both length and breadth with inflation method under cooling by air at 20°C. The biaxially stretched film obtained was about 450 mm in its width and about 57 μm in its thickness.

Example 6

A biaxially stretched film was produced in the same way as that employed in Example 5 except that resin E which is EVA containing 7.5 weight% of vinylacetate content (DPDJ #8425, manufactured by Nippon Unicar Co., Ltd.) was used as inner layer.

Example 7

A biaxially stretched film was produced in the same way as that employed in Example 5, except that resin E was used as outer layer and the temperature of hot wind in the hot wind cylinder was 95°C.

Example 8

A biaxially stretched film was produced in the same way as that employed in Example 5, except that resin F which is a ethylene-methylmethacrylate copolymer resin containing 12.0 weight% of methylmethacrylate content (Nucrel N1202, manufactured by Du Pont-Mitsui Co.) with adding 1000 ppm of nonionic antistatic agent (ELEGAN S-100, manufactured by Japan Oil Fats and Co., Ltd.) was used as outer and inner layers and the temperature of hot wind in the hot wind cylinder was 95°C.

Example 9

A biaxially stretched film was produced in the same way as that employed in Example 5, except that resin G which is a ethylene-acrylic acid copolymer resin containing 6 weight% of acrylic acid content (Escore #TR5001, manufactured by Exxon Company, melt index = 2.0, density = 0.93 g/cm³, melting point = 102°C) with adding 1000 ppm of nonionic antistatic agent (ELEGAN S-100, manufactured by Japan Oil and Fats Co., Ltd.) was used as outer and inner layers and the temperature of hot wind in the hot wind cylinder was 95°C.

Example 10

A biaxially stretched film was produced in the same way as that employed in Example 5, except that resin H which is a copolymer nylon 6~12 (CM6541X3, manufactured by Toray Industries Inc., density = 1.06, melting point = 130°C) was used as outer layer and resin I which is an acid grafted EVA (E-100H, manufactured by Mitsubishi Petrochemical Co., Ltd., melt index = 2.3, density = 0.94, melting point = 93°C) was used as adhesive layer.

Example 11

A biaxially stretched film was produced in the same way as that employed in Example 5, except that resin J which is a linear low density polyethylene (UZ1030L, manufactured by Mitsui Petrochemical Industries, Ltd., melt index = 3.0, melting point = 120°C, density = 0.910) was used as sealing layer.

Example 12

A biaxially stretched film was produced in the same way as that employed in Example 5, except that resin K described in Example 2 was used as oxygen gas barrier layer.

Example 13

A biaxially stretched film was produced in the same way as that employed in Example 5, except that resin L which is a ethylene-1,4-diene copolymer resin (ROP2D, manufactured by Mitsubishi Petrochemical Co., Ltd., melt index = 2.6, density = 0.923 g/cm³) was used as outer layer and the irradiation dose was changed to 6 Mega rad.

Example 14

A biaxially stretched film was produced in the same way as that employed in Example 5, except that following resin Q was used as an oxygen gas barrier layer. The resin Q is a blended resin consisting of 30 weight% of terephthalic acid-ethylene glycol-1,4-cyclohexane dimethanol copolymer (Kodar PETG, manufactured by

Eastman Kodak Co.) as polyester resin, 30 weight% of HYTREL #2501 as polyester elastomer, 40 weight% of vinylidene chloride-methylacrylate copolymer resin (94 weight%, vinylidene chloride content), and 2 weight% of epoxidized soybean oil to said copolymer resin.

5 Construction of film layers and test results on physical properties obtained in Example 5~14 are shown in Table 2.

Comparative Example 6

10 A biaxially stretched film was produced in the same way as that employed in Example 5, except that following resin M was used as oxygen gas barrier layer. The resin M is a blended resin consisting of 80 weight% of PIFG-40 as polyester resin, 15 weight% of HYTREL #2501 as polyester elastomer, 5 weight% of vinylidene chloridemethylacrylate copolymer resin (94 weight%, vinylidene chloride content), and 2 weight% of epoxidized soybean oil to said copolymer resin.

Comparative Example 7

15 A biaxially stretched film was produced in the same way as that employed in Example 5, except that following resin N was used as oxygen gas barrier layer. The resin N is a blended resin consisting of 30 weight% of PIFG-40 as polyester resin, 10 weight% of HYTREL #2501 as polyester elastomer, 60 weight% of vinylidene chloride-methylacrylate copolymer resin (94 weight%, vinylidene chloride content), and 2 weight% of epoxidized soybean oil to said copolymer resin.

Comparative Example 8

25 A biaxially stretched film was produced in the same way as that employed in Example 5, except that resin O was used as oxygen gas barrier layer. The resin O is a blended resin consisting of 60 weight% of Kodar PETG as polyester resin, 40 weight% of vinylidene chloride-methylacrylate copolymer resin (94 weight%, vinylidenechloride content), and 2 weight% of epoxidized soybean oil to said copolymer resin.

Comparative Example 9

A biaxially stretched film was produced in the same way as that employed in Example 5, except that resin S described in Comparative Example 1 was used as oxygen gas barrier layer.

Comparative Example 10

35 A biaxially stretched film was produced in the same way as that employed in Example 5, except that resin P was used as oxygen gas barrier layer. The resin P is a blended resin consisting of 60 weight% of HYTREL #2501 as polyester elastomer, 40 weight% of vinylidene chloride-methylacrylate copolymer resin (94 weight%, vinylidene chloride content), and 2 weight% of epoxidized soybean oil to said copolymer resin.

Comparative Example 11

45 A biaxially stretched film was produced in the same way as that employed in Example 5, except that resin R which dispersed 2 weight% of epoxidized soybean oil into vinylidene chloride-methylacrylate copolymer resin (94 weight%, vinylidene chloride content) as oxygen gas barrier layer, was used.

Comparative Example 12

50 Film constitution was the same constitution as that employed in Example 5 and the sample was prepared by stretching without electron beam irradiation. The stretching was carried out to pass through hot water bath at 80~85°C and hot wind cylinder at 100°C, then the 2.3 times stretching was done in both direction of length and breadth respectively with inflation method while cooling by air at 20°C. The obtained biaxial stretching film shows 345 mm in its flat width and 96 µm in its thickness.

55 Further, the inflation method which was the same stretching condition (hot water bath: 80~95°C, 110°C in wind cylinder) of Example 5, could not apply for this sample.

Constitution of film layers and measured results on physical properties obtained in Comparative Example 6~12 was shown in Table 3.

Table 4 shows the method to determine the physical properties. In this Table, the value of gel% in polyolefin layer was determined on the polyolefin layer separated from biaxially stretched film.

According to this invention, laminated film having various excellent properties on heat resistance sealing property, melt hole resistance, cold resistance, and transparency was obtained as shown apparently in Example 5~14.

The laminated film being fitted to the object of this invention should show below 1 of damage number in melt hole resistance, O in cold resistance, over 15% in heat shrinkage percentage, below 8% in haze, below 200 cc/m²-day-atm in oxygen gas transmission rate, over B in colouring, over 1.8 kg/15 mm in sealing strength, and no-cutting in melting at the sealing portion.

In Comparative Example 6, sufficient oxygen gas barrier property was not obtained because of too small weight ratio of PVDC in intermediate layer.

In Comparative Example 7, weight ratio of PVDC in intermediate layer is too large, so PVDC becomes matrix which cause colouring by decomposition under electron beam irradiation and shows also poor cold resistance.

In Comparative Example 8, suitable amount of polyester elastomer was not contained in intermediate layer, so the improvement on cold resistance could not be attained. And intermediate layer shows colouring with decomposition at coextruding.

In Comparative Example 9, since suitable polyester elastomer was not contained in intermediate layer, the improvement on cold resistance could not be attained.

In Comparative Example 10, intermediate layer was 2 components compatible system consisting of PVDC and polyester elastomer, so oxygen gas barrier property was greatly deteriorated.

In Comparative Example 11, intermediate layer contains only vinylidene chloride polymer, so cold resistance became low and strong colouring was shown by the decomposition under electron beam irradiation.

In Comparative Example 12, as stretching process was carried out without electron beam irradiation, film production was failed to stretch the film by ordinary stretching ratio and inferior sealing strength, cutting of sealing by melting, and melt hole resistance were observed even low stretching ratio due to the lack of crosslinking. Further, since the stretching temperature can not be raised enough, after heat shrinking, the shrinkage of intermediate layer was not sufficient. Therefore the intermediate layer became to wrinkle and the transparency of laminated film was inferior.

Table 2 Example 5 ~ 14

Exam- ple	Construction of laminated film					Irra- dia- tion (Mrad)	Property of laminated film					Gel% of layers			Seal strength (kg/15 mm)	Seal cut- ting
	Seal layer (μ m)	Adhe- sive layer (μ m)	Inner layer (μ m)	Adhe- sive layer (μ m)	Inter- mediate layer (μ m)	Outer layer (μ m)	Melt hole resist- ance *1	Cold resist- ance	Heat shrinkage percentage L/T (%)	Haze (%)	Oxygen gas trans- mission rate *2	Colu- ring	Outer layer (%)	Inner layer (%)	Seal layer (%)	
5	C (13)	D (1)	B (20)	D (1)	A (8)	D (1)	0	O	52/55	4.5	70	A	55	50	25	*3 O
6	C (13)	D (1)	E (20)	D (1)	A (8)	D (1)	0	O	55/57	4.0	70	A	55	62	25	O
7	C (13)	D (1)	E (20)	D (1)	A (8)	E (13)	0	O	58/59	3.5	70	A	62	62	25	O
8	C (13)	D (1)	F (20)	D (1)	A (8)	F (13)	0	O	58/60	3.5	70	A	65	60	25	O
9	C (13)	D (1)	G (20)	D (1)	A (8)	G (13)	0	O	55/56	4.0	70	A	50	45	25	O
10	C (13)	I (1)	B (20)	I (1)	A (8)	H (13)	0	O	50/47	3.5	65	A	20	50	25	O
11	J (13)	D (1)	B (20)	D (1)	A (8)	B (13)	0	O	53/56	3.0	70	A	55	50	20	O
12	C (13)	D (1)	B (20)	D (1)	K (8)	B (13)	0	O	55/56	3.5	65	A	55	50	25	O
13	C (13)	D (1)	B (20)	D (1)	A (8)	L (13)	0	O	53/55	3.5	70	A	65	40	10	O
14	C (13)	D (1)	B (20)	D (1)	Q (8)	B (13)	0	O	53/55	4.0	80	B	55	50	25	O

*1: (damage numbers in 5 sheets) *2: (cc/m²·day·atm) *3: O; no cutting in melt. X; cutting in melt.

Table 3 Comparative Example 6 ~ 12

Com- para- tive Exam- ple	Construction of laminated film						Irra- dia- tion (Mrad)	Property of laminated film					Gel% of layers			Seal strength (kg/15 mm)	Seal cut- ting *3	
	Seal layer (μ m)	Adhe- sive layer (μ m)	Inner layer (μ m)	Adhe- sive layer (μ m)	Inter- mediate layer (μ m)	Outer layer (μ m)		Melt hole resist- ance *1	Cold resist- ance	Heat shrinkage percentage L/T (%)	Haze (%)	Oxygen gas trans- mission rate *2	Colu- m ring	Outer layer (%)	Inner layer (%)			Seal layer (%)
6	C (13)	D (1)	B (20)	D (1)	M (8)	D (1)	B (13)	0	O	52/52	3.0	280	A	55	50	25	2.0	O
7	C (13)	D (1)	B (20)	D (1)	N (8)	D (1)	B (13)	0	x	55/53	3.5	50	C	55	50	25	2.1	O
8	C (13)	D (1)	B (20)	D (1)	O (8)	D (1)	B (13)	0	x	50/49	4.0	70	C	55	50	25	2.0	O
9	C (13)	D (1)	B (20)	D (1)	S (8)	D (1)	F (13)	0	x	54/56	3.0	40	A	55	50	25	2.0	O
10	C (13)	D (1)	B (20)	D (1)	P (8)	D (1)	B (13)	0	O	57/60	20	220	A	55	50	25	2.2	O
11	C (13)	D (1)	B (20)	D (1)	R (8)	D (1)	B (13)	0	x	49/50	3.5	20	C	55	50	25	2.0	O
12	C (13)	D (1)	B (20)	D (1)	A (8)	D (1)	B (13)	4	O	35/40	43	60	A	0	0	0	1.3	x

*1: (damage numbers in 5 sheets) *2: (cc/m²·day·atm) *3: O; no cutting in melt. X; cutting in melt.

Table 4

Item of test	Method of determination
Heat shrinking percentage	Measurement is carried out using 20 pieces of film with 10 cm x 10 cm, which is immersed into hot water for 10 second at 90°C under free shrinking. Then shrinking is calculated against both original length and breadth and reported with average value.
Impact thrusting energy	Measurement is carried out using film with 40 µm in thickness, following ASTM-D3763 at 5°C of ambient temperature with Impact Tester (Rheometrics Dropweight Tester # Model PDT-5000).
Melt hole resistance	A hole having an internal diameter of 20 mm and a depth of 20 mm is covered with a film which is pressed by a seal packing. After the hole has been evacuated to 10 Torr, the hole is immersed in hot water at 85°C for 10 seconds. The number of the sheet pierced with hole when 5 sheets of film are subjected to this treatment is determined.

<p>Oxygen gas transmission rate</p>	<p>Prior to the test, the film is left for 1 week in controlled room with 100%RH, at 30°C. The measurement is carried out with ^RMOCON # OX-TRAN TWIN (coulometric detection) designated by ASTM D-3985-81, under 100%RH, at 30°C.</p>
<p>Gel fraction (%)</p>	<p>(1) Gel fraction, %, of polyolefin Sample, weight (W_1) is immersed for 2 hours into trichlorobenzene kept at 135°C, then unsolved substance is separated using 100 mesh stainless wire sieve. The residue is dried in vacuum for 24 hours, at 40°C and its weight (W_2) is measured and the fraction is calculated by following equation.</p> $\text{Gel fraction (\%)} = (W_2/W_1) \times 100$ <p>(2) Gel fraction, %, of polyamide Measurement is carried out by the same method in case of polyolefin, except immersion into metacresol kept at 70°C, for 2 hours.</p>

5 Cold resistance	Measurement is carried out to determine the change of oxygen barrier property with pinhole, after abuse treatment based upon U.S. MIL-B-131 and FED. TEST METHOD STD No. 101C. The abuse treatment is done by GELVO FLEX TEST with tubular film having 90 mm in diameter and 200 mm in length. A thousand times of a series of crushing, bending, and rotating are added to tubular film with 40 (cycles/min) and 440° (arc) under ambient temperature of -10°C. Then, oxygen gas transmission rate is evaluated on the opened tubular film with rating O for no change before and after the abuse and rating X for deterioration of more than 400 cc/m ² ·day·atm.
40 Haze (%)	Measurement is carried out for the laminated film with 10 cm × 10 cm to shrink freely for 1 minute in hot water at 90°C and haze (%) is determined with Haze Meter, type MDHΣ 80 manufactured by Nihon Denshoku Kogyo K.K.

5 10 15 20	Colouring on laminated film (Colouring)	Measurement is carried out with 3 rating, after laminated film 10 cm × 10 cm is immersed and shrunken freely for 1 minute in boiling water. A Colouring is not visually observed. B Slight colouring, but no problem for practical use. C Extensive colouring, can not be used practically.
25 30 35	Seal strength	Measurement is carried out with cutting the film into long strip with 15 mm width to meet at right angle to seal line, opening said strip, setting to the chuck of tensile tester placing seal line center, drawing with 200 mm/min., and reading the tenacity at the cutting seal line.

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5 Cutting by
melting

Measurement is carried out with using vacuum chamber (# Vc 999), raising the temperature at sealing with hitting 20 times using impulse seal (2.5 graduation) and attaining equilibrium (210°C, peak temperature), executing sealing on the film, and evaluating the cutting by melting. Cutting by melting means being cut at seal line, even in a portion.

Claims

1. A resin composition which comprises:
 - (i) 26 to 70 weights of a thermoplastic polyester resin;
 - (ii) 10 to 30 weight% of a polyester elastomer; and
 - (iii) 20 to 44 weight% of a vinylidene chloride resin.
2. A composition according to claim 1 wherein the thermoplastic polyester resin comprises a mixed dibasic acid component comprising terephthalic acid and isophthalic acid, and a mixed dialcohol component comprising ethylene glycol and diethylene glycol.
3. A composition according to claim 1 or 2 wherein the polyester elastomer comprises a mixed dibasic acid component comprising terephthalic acid and isophthalic acid, and a mixed dialcohol component comprising 1,4-butanediol and polytetramethylene glycol.
4. A biaxially stretched heat shrinkable film having an oxygen gas barrier property which comprises a composition as defined in any one of the preceding claims.
5. A biaxially stretched heat shrinkable laminated film having a heat shrinkage percentage of over 15% at 90°C and an oxygen gas barrier property, which comprises an intermediate oxygen gas barrier layer comprising a composition as defined in any one of claims 1 to 3, an outer layer of a polyamide or crosslinkable polyolefin, an inner layer of the same crosslinkable polyolefin used in the outer layer or a different polyolefin, and a heat sealing layer of a low crosslinkable polyolefin, at least the outer layer, the inner layer and the heat sealing layer being crosslinked by electron beam irradiation.
6. A film according to claim 5 wherein the crosslinkable polyolefin is at least one of an ethylene-vinylacetate copolymer resin, ethylene-acrylic acid copolymer resin, ethylene-methacrylic acid copolymer resin, ethylene-acrylic acid ester copolymer resin, ethylene-methacrylic acid ester copolymer resin, ethylene-acrylic acid allyl copolymer resin, ethylene-vinyl acetate-acrylic acid allyl copolymer resin, ethylene-1,4-diene copolymer resin, ethylene-propylene-1,4-diene copolymer resin, linear low density polyethylene obtainable by gas phase polymerization and ionomer resin.

7. A film according to claim 5 or 6, wherein the low crosslinkable polyolefin is at least one of a linear low density polyethylene obtainable by solution polymerization, ethylene-propylene copolymer resin, propylene-butene copolymer resin and low density polyethylene.
- 5 8. A film according to any one of claims 5 to 7 wherein adhesive layers are disposed between each of the outer layer, the intermediate layer, the inner layer and the heat sealing layer.
9. A process for producing a film as defined in claim 4 which comprises extruding the composition to form a film and biaxially stretching the film.
- 10 10. A process for producing a film as defined in any one of claims 5 to 9 which comprises coextruding the compositions forming the respective layers to form a film, crosslinking the layers by means of electron beam irradiation, preferably at 1 to 12 Mega rad, and biaxially stretching the film.
- 15 11. Use of a film as defined in any one of claims 4 to 8 in packaging an article.

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(54) **Resin composition and heat shrinkable film comprising the same composition layer.**

(57) A resin composition which comprises :
(i) 26 to 70 weight% of a thermoplastic polyester resin ;
(ii) 10 to 30 weight% of a polyester elastomer ;and
(iii) 20 to 44 weight% of a vinylidene chloride resin.

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EUROPEAN SEARCH REPORT

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DOCUMENTS CONSIDERED TO BE RELEVANT			
Category	Citation of document with indication, where appropriate, of relevant passages	Relevant to claim	CLASSIFICATION OF THE APPLICATION (Int. Cl.5)
A	WO-A-8 602 483 (ERCON INC.) * page 6, line 1 - line 5; claim 1 *	1,2	C08L67/02 C08L27/08 B32B27/36 /(C08L67/02, 27:08)
A	FR-A-2 371 348 (E.I.VALYI) * page 6, line 7 - line 20 *	5	
A	DE-A-3 207 742 (REHAU PLASTIKS AG) * claims 1,3,7 *	5,6	
D,A	US-A-3 741 253 (H.J.BRAX) * claims 1,4 *	5,6,11	
			TECHNICAL FIELDS SEARCHED (Int. Cl.5)
			B32B C08L C08J
The present search report has been drawn up for all claims			
Place of search BERLIN		Date of completion of the search 04 MAY 1993	Examiner ANGIOLINI D.
<p>CATEGORY OF CITED DOCUMENTS</p> <p>X : particularly relevant if taken alone Y : particularly relevant if combined with another document of the same category A : technological background O : non-written disclosure P : intermediate document</p> <p>T : theory or principle underlying the invention E : earlier patent document, but published on, or after the filing date D : document cited in the application L : document cited for other reasons & : member of the same patent family, corresponding document</p>			

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